


 Innovation and Equipment	MODIFIED STARCH FLASH DRYER PROJECT						
	FAN CALCULATION						
	Project No.	Discipline	Document Type	Plant / Equipment No	Sequence No.	Rev.	
	5204	CL	PR	000	04	00	

# FLASH DRYER



## FAN CALCULATION

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<b>REV.</b>	<b>ISSUE</b>	<b>PURPOSE OF ISSUE</b>	<b>PREPARED</b>	<b>CHECKED</b>	<b>APPROVED</b>

	MODIFIED STARCH FLASH DRYER PROJECT						
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	5204	PR	CL	000	04	00	

## TABLE OF CONTENT

1. Centrifugal Fan Calculation.....	3
1.1. Fan Air Volume .....	3
1.2. Pressure Drop .....	4
1.3. Fan Motor Power .....	10
1.4 Summary .....	11

	MODIFIED STARCH FLASH DRYER PROJECT						
	FAN CALCULATION						
	Project No.	Discipline	Document Type	Plant / Equipment No	Sequence No.	Rev.	
	5204	PR	CL	000	04	00	

## 1. Centrifugal Fan Calculation

### 1.1. Fan Air Volume

The required air volume or flow of the centrifugal fan are calculated in sections 1.3 and 1.4:

$$Q_s = Ma \cdot \Delta H$$

Where:

$Ma$ : Mass of air, kg/h

$\Delta H$ : Change in enthalpy of air:  $H_o - H_i$

$H_i$ : Enthalpy of air (Outlet air temp. 55 °C, 43 % Moisture)

$H_o$ : Enthalpy of air (after heater 170 °C, 1% Moisture)

Hence:

$$Ma = ra \cdot Va$$

$ra$ : Density of air, kg/m<sup>3</sup>

$Va$ : Volume of air, m<sup>3</sup>/h



$$7,739,363,411 = Ma \cdot (319768 - 171430)$$

$$Ma = 52,174 \text{ Kg/h}$$

$$53,121 = 0.78 \times Va$$

$$Va = 66,890 \text{ m}^3/\text{h}$$

**Required Air Volume is: 67000 m<sup>3</sup>/h**

 Innovation and Equipment	MODIFIED STARCH FLASH DRYER PROJECT						
	FAN CALCULATION						
	Project No.	Discipline	Document Type	Plant / Equipment No	Sequence No.	Rev.	
	5204	PR	CL	000	04	00	

## 1.2. Pressure Drop

The total pressure loss of the pneumatic system can be expressed as:

$$\Delta P_t = \Delta P_{acc} + \Delta P_g + \Delta P_s + \Delta H_g + \Delta H_s + \Delta P_{misc}$$

$\Delta P_t$ : Total pressure loss in the system

$\Delta P_{acc}$ : Pressure loss due to acceleration of the solids from their "at rest" condition at the pickup point.

$\Delta P_g$ : Friction pressure loss of the gas

$\Delta P_s$ : Friction pressure loss of the solids

$\Delta H_g$ : Elevation pressure loss of the gas

$\Delta H_s$ : Elevation pressure loss of the solid

$\Delta P_{misc}$ : Pressure losses from miscellaneous equipment (cyclone, bag filter)

### 1.2.1. Pressure loss due to acceleration of the solids:

$$\Delta P_{acc} = 6894.8 \frac{W \cdot V_p}{144 \cdot g} \text{ (Pa)}$$

Where:

$W$ : Solids mass velocity, ( $\frac{\text{lbs}}{\text{s.ft}^2}$ )

$V_p$ : Particle velocity, (ft/s)

$g$ : Acceleration due to gravity, (32.2)

Hence:

$$V_p = 0.8V_g$$

$V_g$ : Maximum Air velocity, (ft/s) = 65.6

$$W = \frac{M_s}{A}$$



$M_s$ : Starch feed rate, (lbs/s)

$A$ : Duct Area, ( $\text{ft}^2$ )

$$W = 0.454 \frac{\text{lbs}}{\text{s.ft}^2}$$

$$V_p = 52 \frac{\text{ft}}{\text{s}}$$

$$\Delta P_{acc} = 6894.8 \frac{0.454 \times 52}{144 \times 32.2} = 35.4 \text{ (Pa)}$$

 Innovation and Equipment	MODIFIED STARCH FLASH DRYER PROJECT						
	FAN CALCULATION						
	Project No.	Discipline	Document Type	Plant / Equipment No	Sequence No.	Rev.	
	5204	PR	CL	000	04	00	

### 1.2.2. Friction Pressure loss of the gas:

The frictional pressure drop of the gas is calculated based on the following diagram:

$$\Delta P_g = Fl.L \text{ (Pa)}$$

Where:

*Fl*: Friction loss, from chart, (Pa/m)

*L*: Pipes equivalent length, (m) (From 1.2.3)

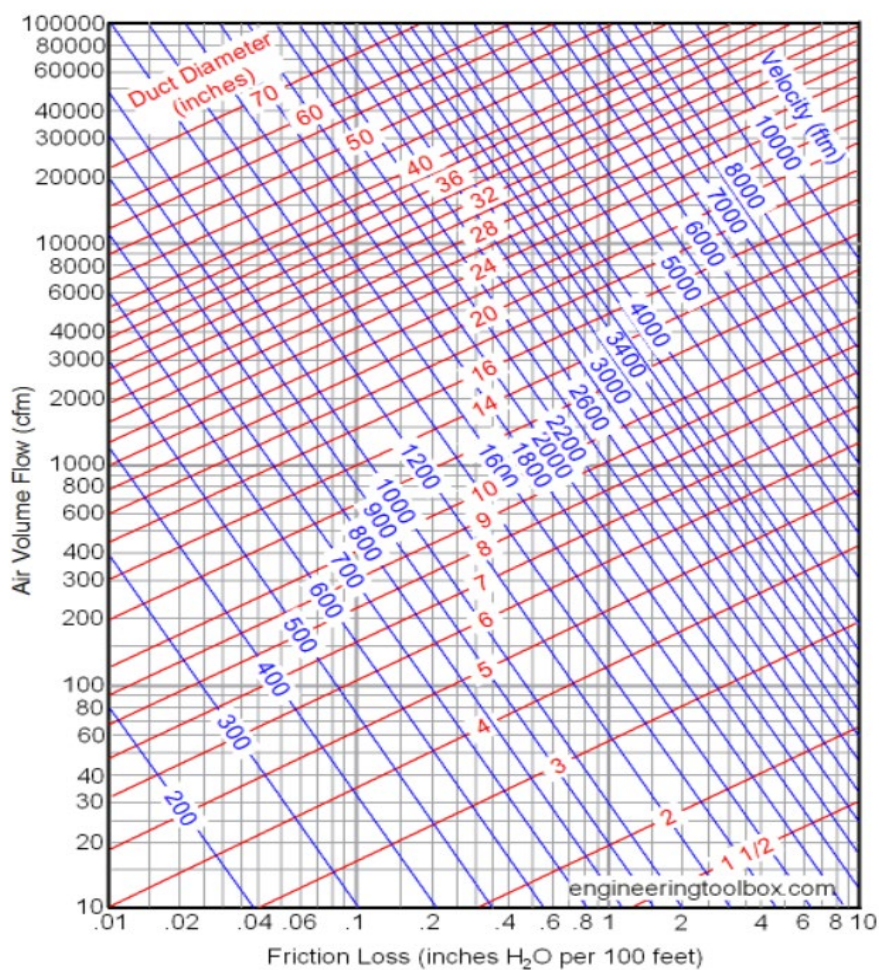




Figure -1

	MODIFIED STARCH FLASH DRYER PROJECT						
	FAN CALCULATION						
	Project No.	Discipline	Document Type	Plant / Equipment No	Sequence No.	Rev.	
	5204	PR	CL	000	04	00	

$$Q = 90000 \frac{m^3}{h} = 52\,950 \text{ CFM}$$

$$\text{Duct Size} = 1300 \text{ mm} = 51 \text{ in}$$

$$Fl = \text{Friction Loss} = 0,2 \frac{\text{Inch H}_2\text{O}}{100 \text{ ft}} = 1,64 \text{ Pa/m}$$

$$L = 282 \text{ m} \quad (\text{From 1.2.3})$$



$$\Delta P_g = Fl \cdot L = 1.64 \times 282 = 463 \text{ (Pa)}$$

### 1.2.3. Pipes equivalent length:

For straight runs use the actual length of the pipe. For bends and other devices, use the table-1 below as a guide:

Table-1

Component	Equivalent Length
Bends, 90° bend, long radius (10 to 1 radius to diameter ratio)	40 x diameter or 20 ft (whichever is larger)
Diverter Valves 45° divert angle 30° divert angle	20 x diameter 10 x diameter
Flexible Hoses Stainless steel, with lined interior Rubber or vinyl hose	3 x pipe length 5 x pipe length
For bends that are less than 90°, use the following equivalent lengths:  $L = 40 \times (\text{Degree of bend} / 90)$	

 Innovation and Equipment	MODIFIED STARCH FLASH DRYER PROJECT						
	FAN CALCULATION						
	Project No.	Discipline	Document Type	Plant / Equipment No	Sequence No.	Rev.	
	5204	PR	CL	000	04	00	

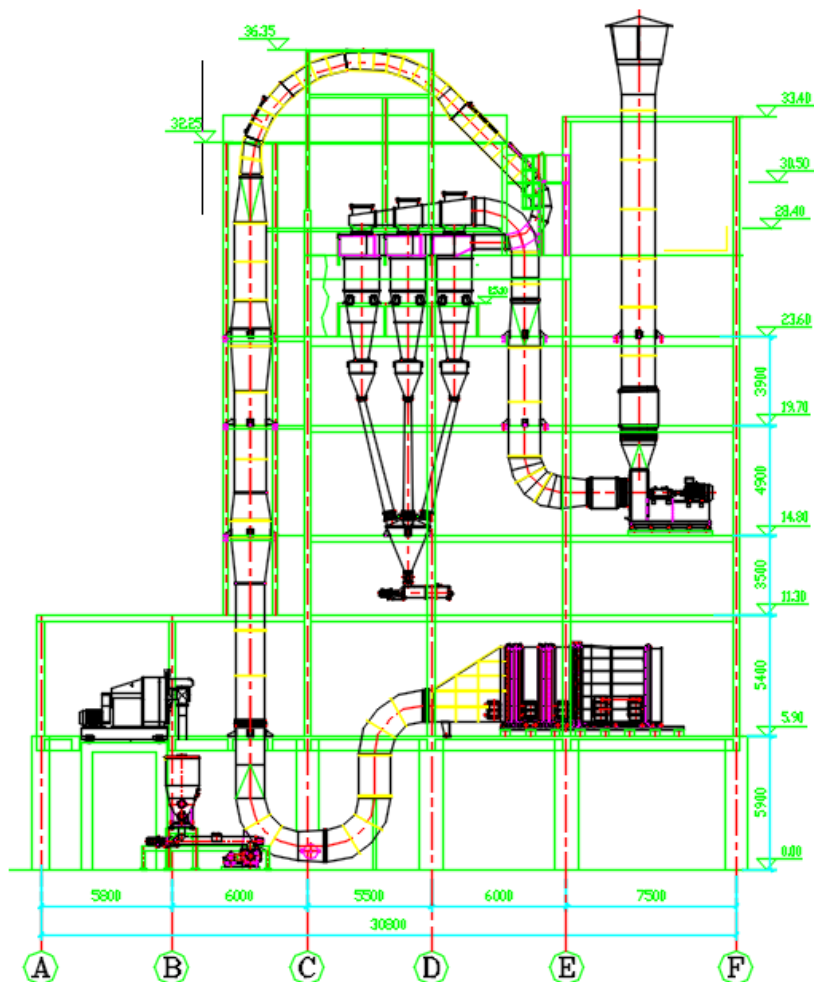




Figure -2

Table -2 (Duct Equivalent Calculation)

Component	Quantity	Max. Diameter (ft)	Equivalent Lenth (ft)	Equivalent Lenth (m)
Bend 90	6	4.59	184	61
Flexible Hoses	2	4.59	91.8	30
Straight Length				50
<b>Total</b>				<b>141</b>

 Innovation and Equipment	MODIFIED STARCH FLASH DRYER PROJECT						
	FAN CALCULATION						
	Project No.	Discipline	Document Type	Plant / Equipment No	Sequence No.	Rev.	
	5204	PR	CL	000	04	00	

$$\text{Safety Factor} = 2$$

$$\text{Total Duct Length} = 2 \times 141$$

$$\text{Total Duct Length} = 282 \text{ m}$$

#### 1.2.4. Friction pressure loss of the solids:

$$\Delta P_s = \Delta P_g \cdot K \cdot R \quad (Pa)$$

Where:

$\Delta P_g$ : Friction pressure loss of the gas (Pa) (From 1.2.2)

$K$ : Friction multiplier for the solids conveyed = 10

$R$ : Solids to gas mass flow ratio, (lb/lb)

$$\text{Hence: } R = \frac{W}{V_p \cdot \rho}$$

$W$ : Solids mass velocity,  $\frac{lb}{s \cdot ft^2}$

$V_p$ : Particle velocity, ft/s

$\rho$ : Air density (lb/ft<sup>3</sup>)

$W$ : Starch Feed Rate / Duct Area,  $\frac{lb}{s \cdot ft^2}$



$$W = \frac{10600 \times \frac{2.2}{3600}}{3.14 \times \frac{4.27^2}{4}} = 0.454$$

$$V_p = (0.8 \times 20 \times 3.28) = 52$$

$$\rho = 0.048$$

$$R = \frac{W}{V_p \cdot \rho} = \frac{0.454}{52 \times 0.048} = 0.179$$

$$\Delta P_s = 463 \times 10 \times 0.179 = 828.77 \quad (Pa)$$

 Innovation and Equipment	MODIFIED STARCH FLASH DRYER PROJECT						
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	Project No.	Discipline	Document Type	Plant / Equipment No	Sequence No.	Rev.	
	5204	PR	CL	000	04	00	

#### 1.2.5. Elevation pressure loss of the gas:

$$\Delta H_g = 6894.8 \frac{\Delta Z \cdot \rho \cdot g}{144 \cdot g_c} \text{ (Pa)}$$

Where:

$\Delta H_g$ : Elevation pressure loss of the gas, (Pa)

$\Delta Z$ : Elevation change in pipeline, (ft)

$\rho$ : Air density, (lb/ft<sup>3</sup>)

$g$ : Acceleration due to gravity = 32.2

$g_c$ : Constant = 32.174

$\Delta Z = 30 \text{ m} = 98 \text{ ft}$

$\rho = 0.048$

$$\Delta H_g = 6894.8 \frac{\Delta Z \cdot \rho \cdot g}{144 \cdot g_c} = 6894.8 \times \frac{98 \times 0.048 \times 32.2}{144 \times 32.174} = 226 \text{ (Pa)}$$

#### 1.2.6. Elevation pressure loss of the solids:

$$\Delta H_s = 6894.8 \frac{\Delta Z \cdot W \cdot g}{144 \cdot V_p \cdot g_c} \text{ (Pa)}$$

Where:

$\Delta H_s$ : Elevation pressure loss of the solids, (Pa)

$\Delta Z$ : Elevation change in pipeline, (ft)



$W$ : Solids mass velocity, ( $\frac{\text{lbs}}{\text{s} \cdot \text{ft}^2}$ )

$V_p$ : Particle velocity, (ft/s)

$g$ : Acceleration due to gravity = 32.2

$g_c$ : Constant = 32.174

$$\Delta H_s = 6894.8 \frac{\Delta Z \cdot W \cdot g}{144 \cdot V_p \cdot g_c} = 6894.8 \times \frac{98 \times 0.454 \times 32.2}{144 \times 52 \times 32.174} = 41 \text{ (Pa)}$$

 Innovation and Equipment	MODIFIED STARCH FLASH DRYER PROJECT						
	FAN CALCULATION						
	Project No.	Discipline	Document Type	Plant / Equipment No	Sequence No.	Rev.	
	5204	PR	CL	000	04	00	

The total pressure loss of the pneumatic system can be expressed as:

$$\Delta Pt = \Delta P_{acc} + \Delta P_g + \Delta P_s + \Delta H_g + \Delta H_s + \Delta P_{misc}$$

$$\Delta P_{misc} = \Delta P_{cyclone} = 1433 \text{ Pa}$$

$$\begin{aligned} \Delta Pt &= 35.4 + 463 + 828.7 + 226 + 41 + 1432 \\ &= 3026 \text{ Pa} \end{aligned}$$

$$\text{Safety Factor} = 2$$

$$\Delta Pt = 3027 \times 2 = 6052 \text{ Pa}$$

### 1.3. Fan Motor Power

$$P = S.F \frac{V_a \cdot \Delta Pt}{e \cdot 3.6 \times 10^6} \text{ (Kw)}$$

$V_a$ : Fan Air Volume ( $m^3/h$ )

$\Delta Pt$ : Total Pressure Drop (Pa)

$S.F$ : Safety Factor

$e$ : Fan Mechanical and Electrical Efficiency

$$V_a = 67,000 \text{ m}^3/h$$



$$\Delta Pt = 6054 \text{ Pa}$$

$$e = 0.68$$

$$S.F = 1.15$$

$$P = 1.15 \frac{67,000 \times 6052}{0.68 \times 3.6 \times 10^6} = 190 \text{ (Kw)}$$

$$\text{Fan Motor Power} = 190 \text{ (Kw)}$$

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	FAN CALCULATION						
	Project No.	Discipline	Document Type	Plant / Equipment No	Sequence No.	Rev.	
	5204	PR	CL	000	04	00	

#### 1.4. Summary

The summary of calculation is according to below table:

Table -3 (Summary of Calculation)

<b>Pressure Safety Factor</b>	<b>2.00</b>	
<b>Flow Safety Factor</b>	<b>1.15</b>	
<b>Fan Efficiency</b>	<b>0.68</b>	
<b>Total Pressure Drop</b>	<b>3,026</b>	<b>Pa</b>
<b>Fan Power</b>	<b>190</b>	<b>Kw</b>
<b>Fan Air Volume</b>	<b>67,000</b>	<b>m3/h</b>
<b>Fan-Total Pressure</b>	<b>6,052</b>	<b>Pa</b>